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Saitou

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(54) **IMAGE FORMATION APPARATUS**

(71) Applicant: **RISO KAGAKU CORPORATION**, Tokyo (JP)

(72) Inventor: **Mamoru Saitou**, Ibaraki-ken (JP)

(73) Assignee: **RISO KAGAKU CORPORATION**, Tokyo (JP)

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(30) **Foreign Application Priority Data**

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B41J 2/045 (2006.01)

(52) **U.S. Cl.**
CPC ***B41J 2/04573*** (2013.01); ***B41J 2/0456*** (2013.01); ***B41J 2/04526*** (2013.01); ***B41J 2/04581*** (2013.01)

(58) **Field of Classification Search**
CPC .. B41J 2/04526; B41J 2/0456; B41J 2/04561; B41J 2/01; B41J 2/045–2/04598; B41J 2/38; B41J 2/393; B41J 2/029; B41J 2/3935
USPC 347/74, 77, 78, 82, 14
See application file for complete search history.

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Primary Examiner — Geoffrey Mruk
Assistant Examiner — Scott A Richmond
(74) *Attorney, Agent, or Firm* — Greenblum & Bernstein P.L.C.

(57) **ABSTRACT**

Included are: a storage unit configured to store profile data in which the amount of landing deviation and the ejection frequency representing the number of ejections of ink droplets per unit time are associated with each other; a correction judgment unit configured to determine whether to allow ejection timing control in print processing by selecting 30 dots as a unit line in an image, adding up a total volume of ink ejected to the unit line, and comparing the total volume of ejected ink with a predetermined threshold; and an ejection control unit configured to obtain the ejection frequency for ejecting ink at a predetermined time interval, from the total volume of ink ejected in the unit line, calculate the amount of landing deviation from the ejection frequency, and control the ejection timing in accordance with the calculated amount of landing deviation.

6 Claims, 13 Drawing Sheets

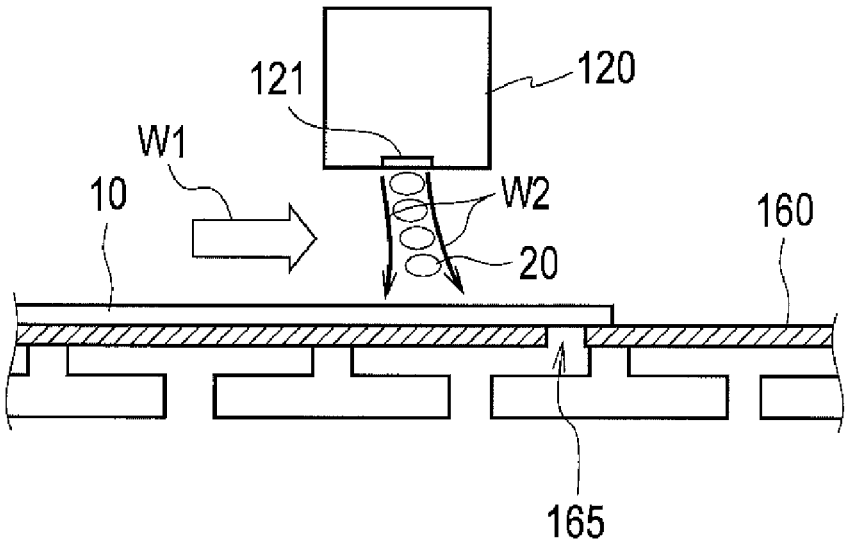

FIG. 1

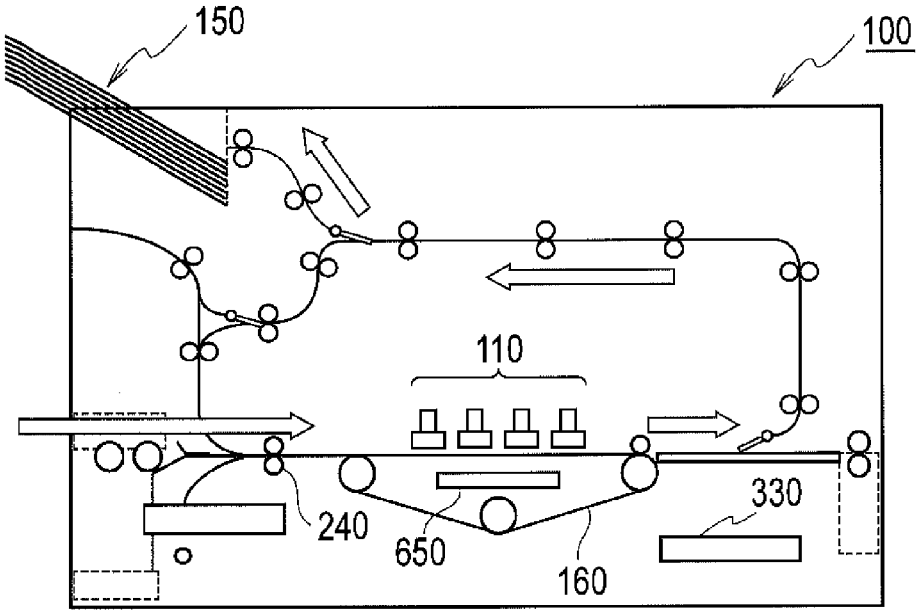
150
100
110
240
650
160
330

FIG. 2

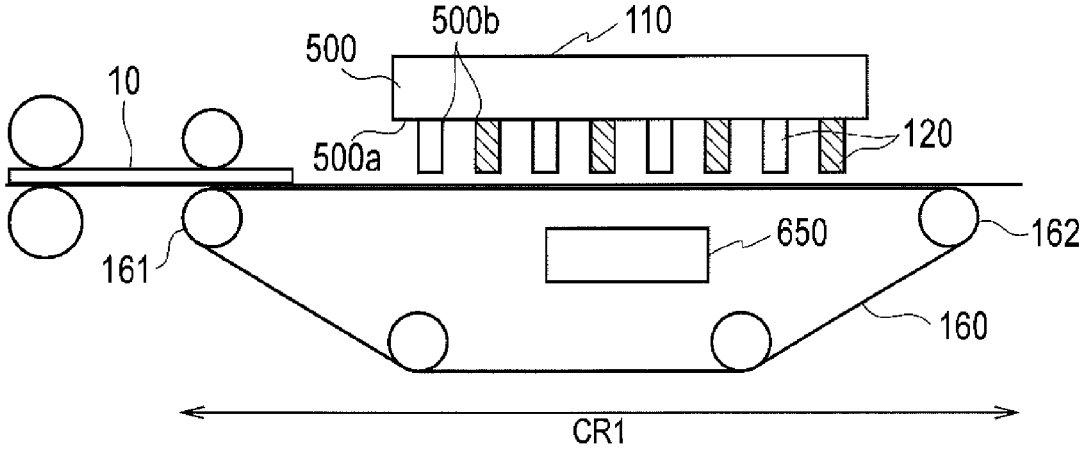
500b
110
500
10
500a
120
650
162
161
160
CR1

FIG. 3A

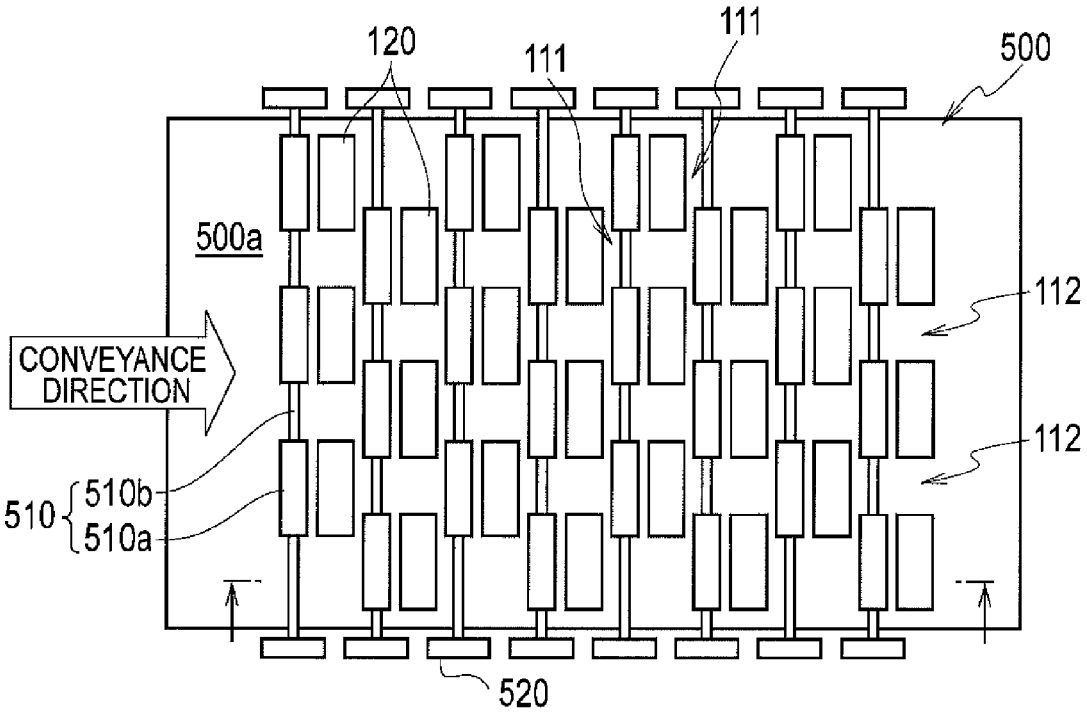
120
111
111
500
500a
112
112
CONVEYANCE DIRECTION
510
510b
510a
520

FIG. 3B

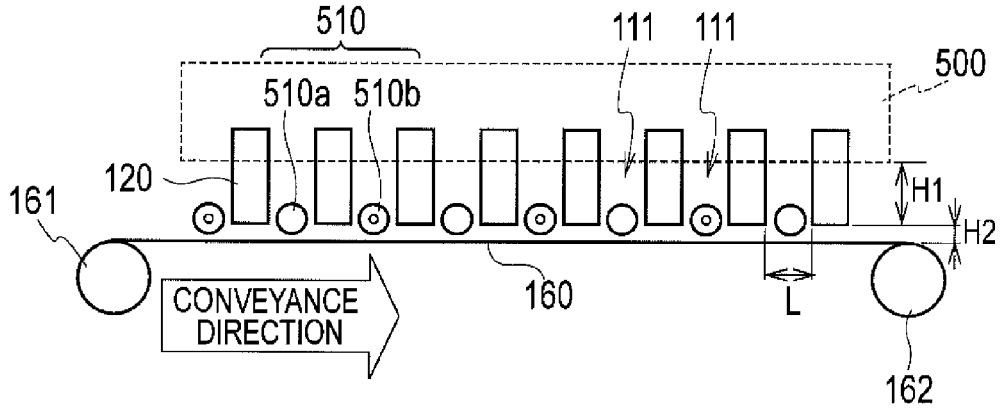
510
111
111
500
510a
510b
120
161
H1
H2
CONVEYANCE DIRECTION
160
L
162

FIG. 4

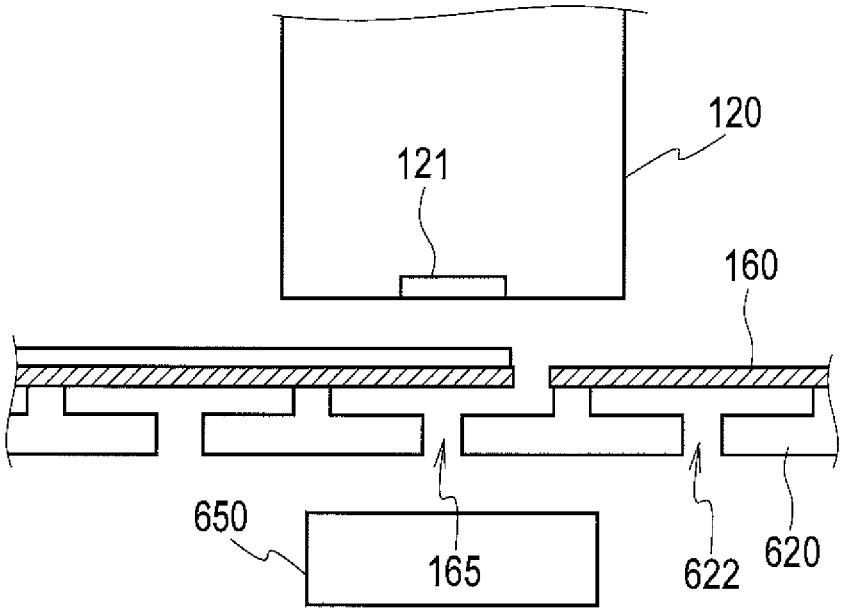

FIG. 5

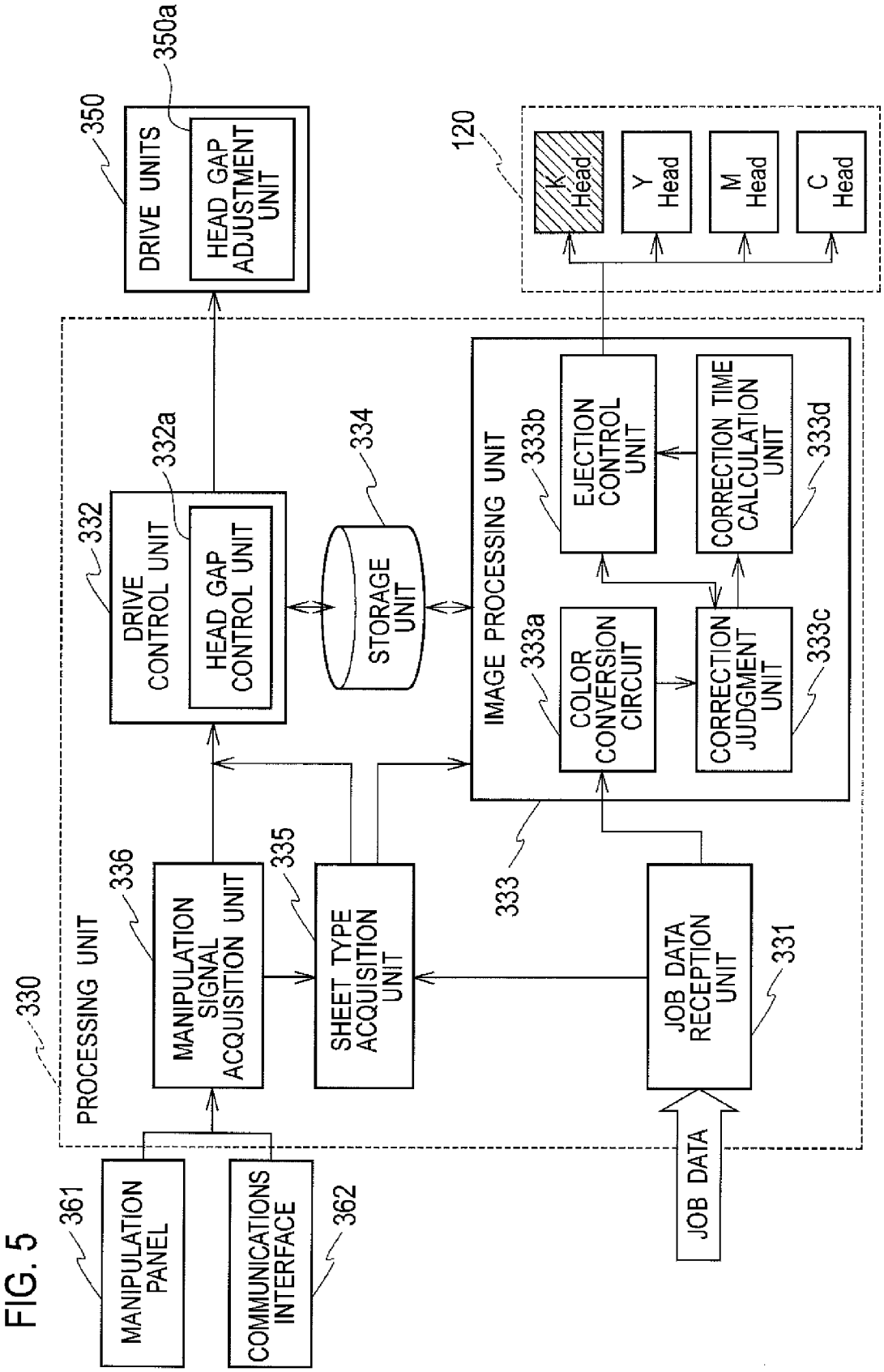
330
PROCESSING UNIT
361
MANIPULATION PANEL
362
COMMUNICATIONS INTERFACE
336
MANIPULATION SIGNAL ACQUISITION UNIT
335
SHEET TYPE ACQUISITION UNIT
331
JOB DATA RECEPTION UNIT
JOB DATA
333
IMAGE PROCESSING UNIT
333a
COLOR CONVERSION CIRCUIT
333b
EJECTION CONTROL UNIT
333c
CORRECTION JUDGMENT UNIT
333d
CORRECTION TIME CALCULATION UNIT
334
STORAGE UNIT
332
DRIVE CONTROL UNIT
332a
HEAD GAP CONTROL UNIT
350
DRIVE UNITS
350a
HEAD GAP ADJUSTMENT UNIT
120
K Head
Y Head
M Head
C Head

FIG. 6

FREQUENCY [Hz]	AMOUNT OF LANDING DEVIATION [μm]	
	HEAD GAP	
	CASE OF 1.6mm	CASE OF 3.0mm
150KHz	18.65	87.69
⋮	⋮	⋮
100Hz	19.13	89.96
⋮	⋮	⋮
1Hz	20.73	98.91

FIG. 7A

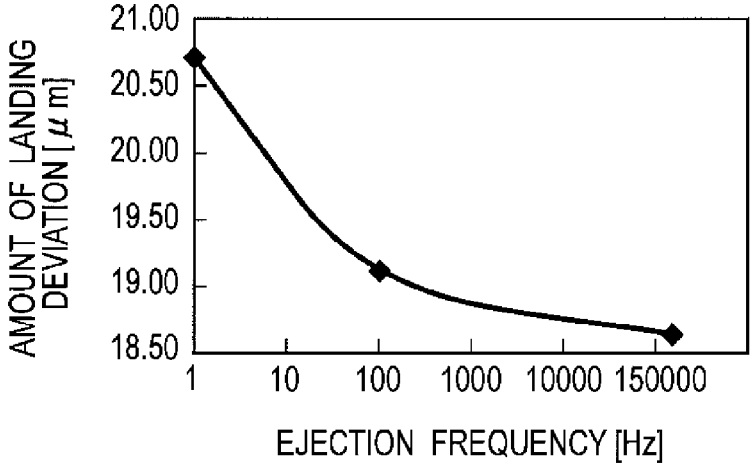

FIG. 7B

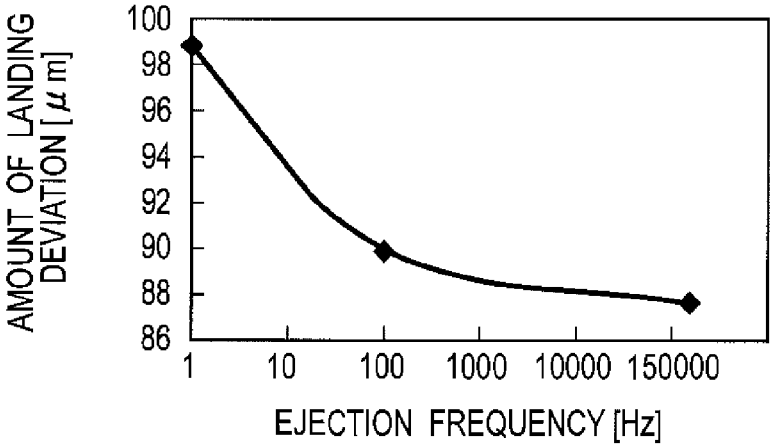

FIG. 8

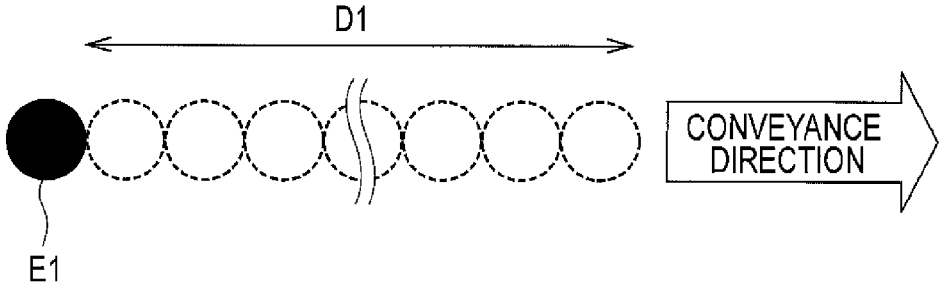

FIG. 9

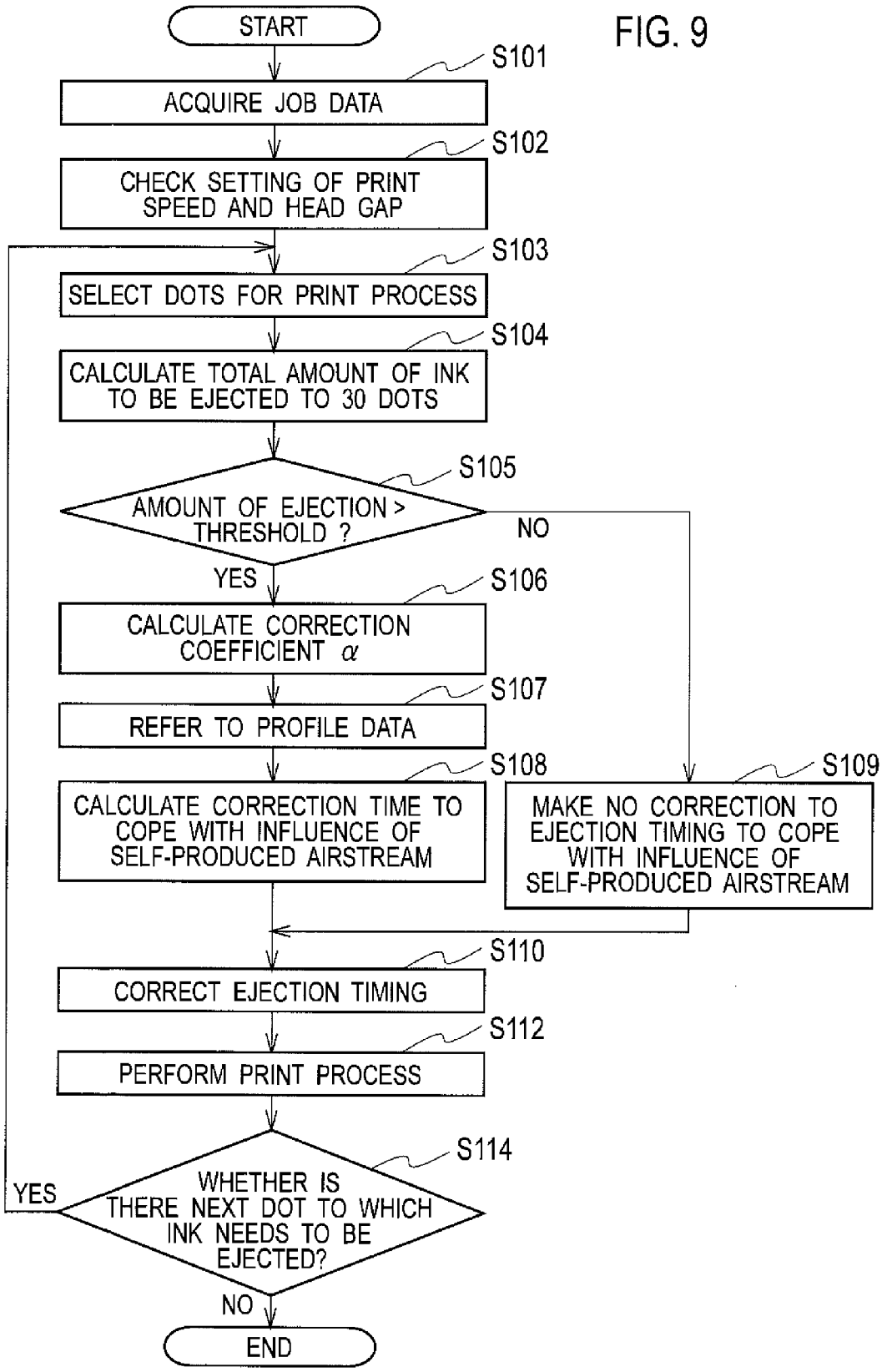
START
S101
ACQUIRE JOB DATA
S102
CHECK SETTING OF PRINT SPEED AND HEAD GAP
S103
SELECT DOTS FOR PRINT PROCESS
S104
CALCULATE TOTAL AMOUNT OF INK TO BE EJECTED TO 30 DOTS
S105
AMOUNT OF EJECTION > THRESHOLD ?
NO
YES
S106
CALCULATE CORRECTION COEFFICIENT α
S107
REFER TO PROFILE DATA
S108
CALCULATE CORRECTION TIME TO COPE WITH INFLUENCE OF SELF-PRODUCED AIRSTREAM
S109
MAKE NO CORRECTION TO EJECTION TIMING TO COPE WITH INFLUENCE OF SELF-PRODUCED AIRSTREAM
S110
CORRECT EJECTION TIMING
S112
PERFORM PRINT PROCESS
S114
WHETHER IS THERE NEXT DOT TO WHICH INK NEEDS TO BE EJECTED?
YES
NO
END

FIG. 10

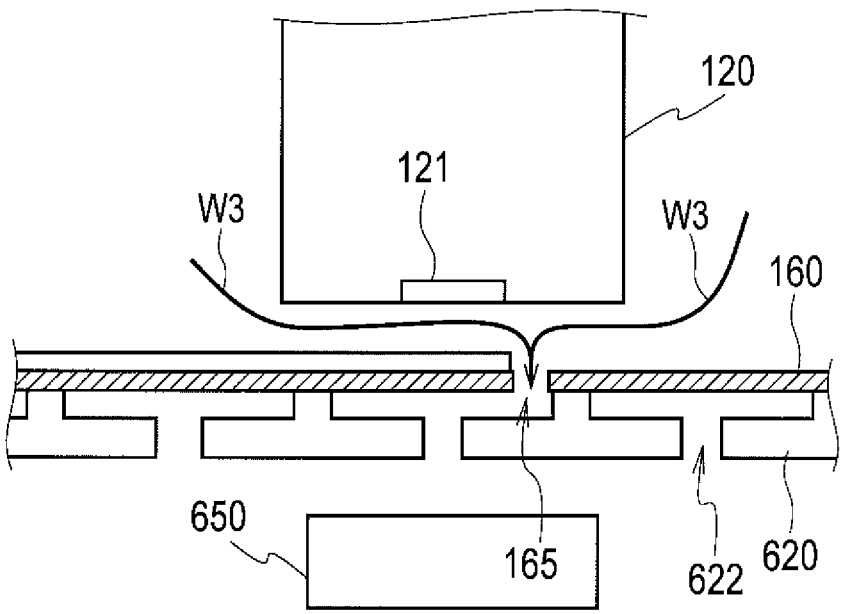

FIG. 11A

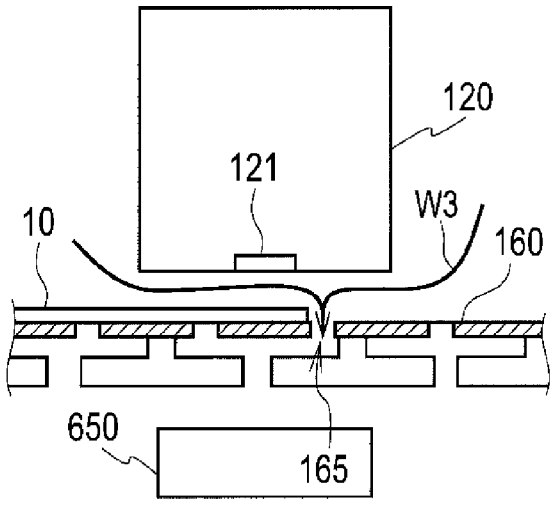

FIG. 11B

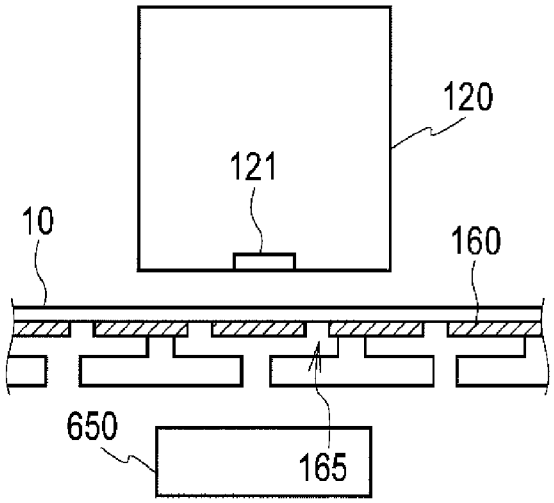

FIG. 11C

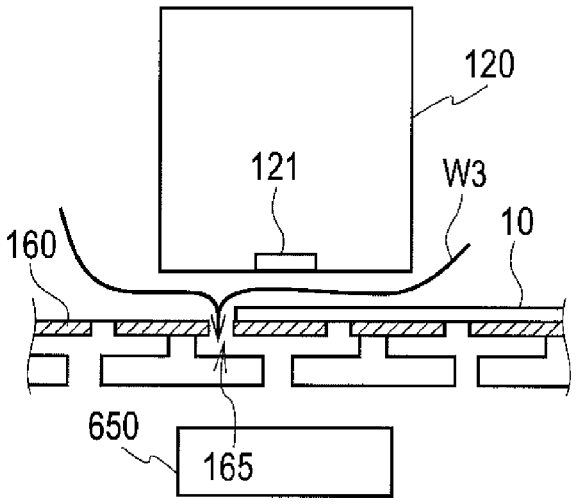

FIG. 12

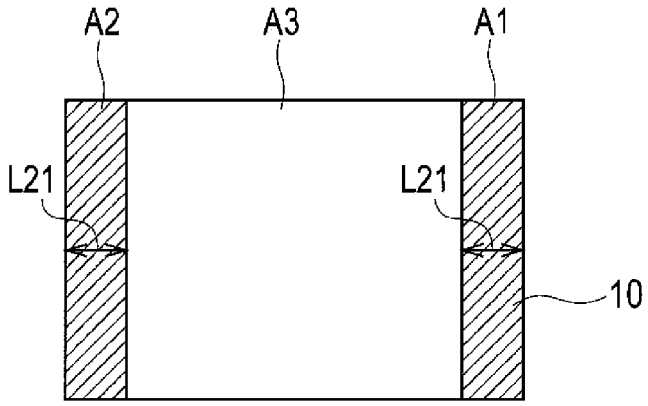

FIG. 13A

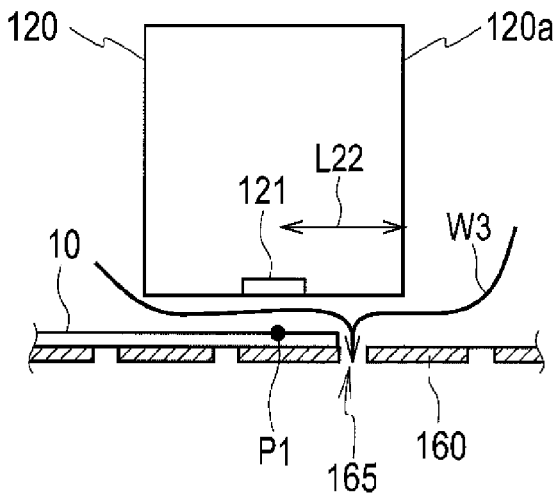

FIG. 13B

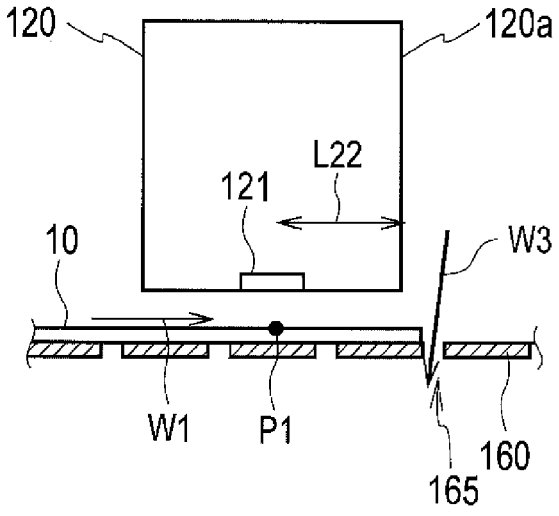

FIG. 14

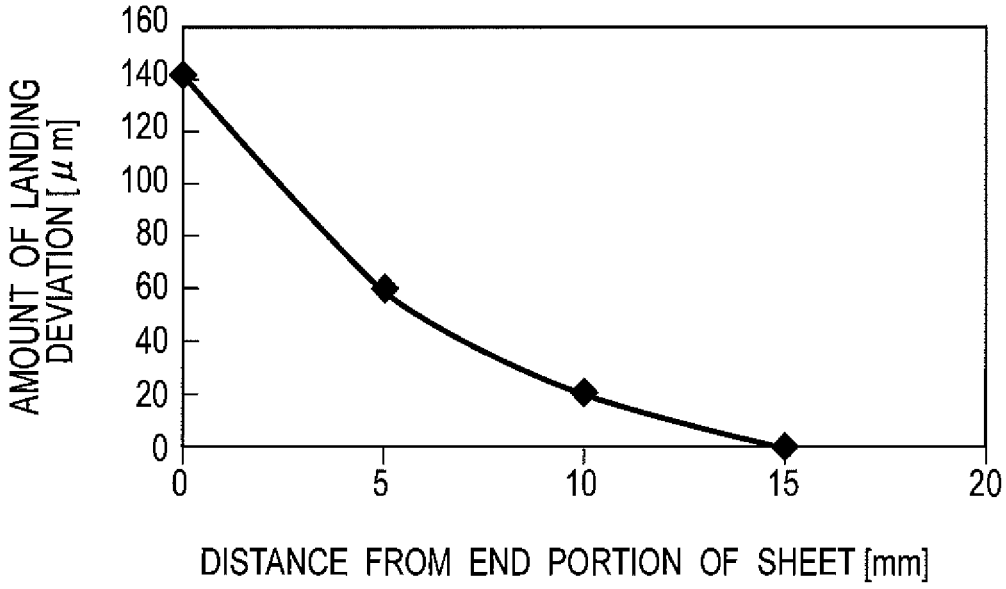
160
140
120
100
80
60
40
20
0
AMOUNT OF LANDING DEVIATION [μm]
0
5
10
15
20
DISTANCE FROM END PORTION OF SHEET [mm]

FIG. 15A

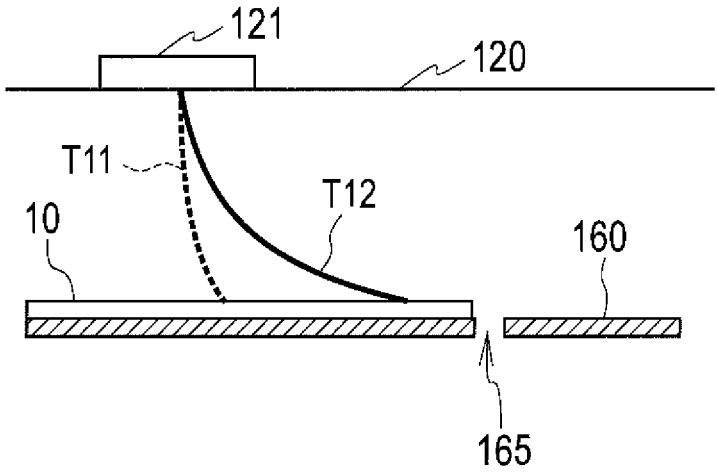

FIG. 15B

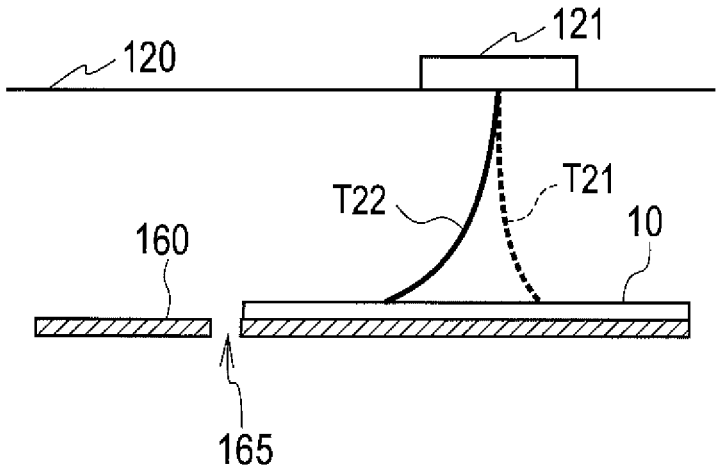

FIG. 16A

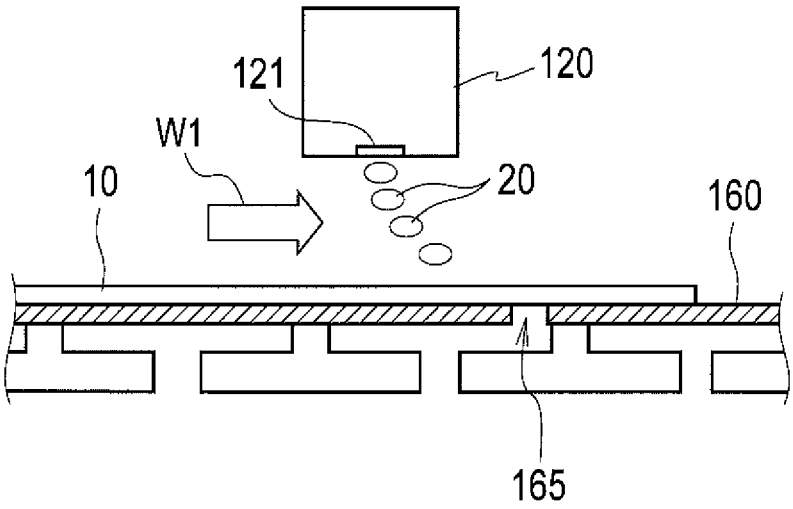

FIG. 16B

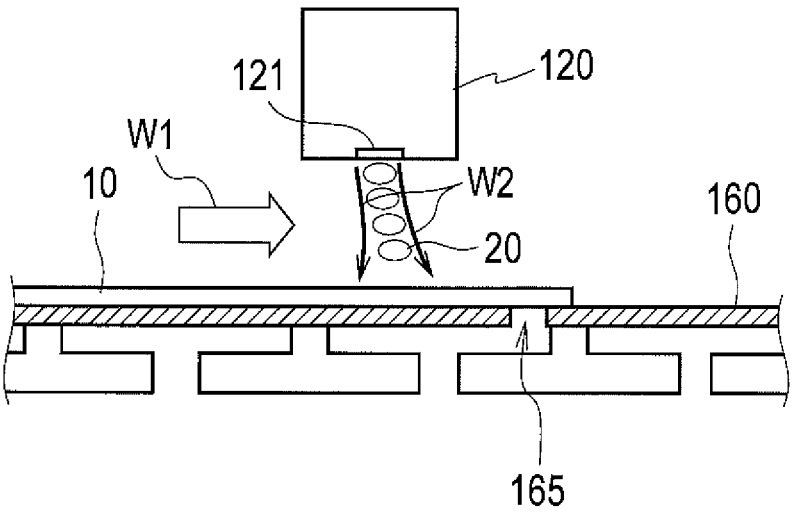

IMAGE FORMATION APPARATUS

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to an image formation apparatus for a printing machine, such as an inkjet image formation apparatus, configured to eject ink onto and thereby form an image on a print sheet being conveyed along a conveyance path.

2. Description of the Related Art

Heretofore, there have been line-type inkjet recording apparatuses as a type of image formation apparatuses. In such a line-type inkjet recording apparatus, a long recording head (line-type long recording head) is used in which ink ejection nozzles are arranged in an array which is as wide as or wider than the width of a print area. Without moving the recording head, the line-type inkjet recording apparatus forms an image by ejecting ink droplets from nozzles of the ink heads onto a recording medium below the ink heads while moving and conveying the recording medium relative to the recording head in a direction crossing the nozzle arrangement direction.

As shown in FIG. **16**A, an airstream W**1** (hereinafter called a conveyance airstream) flowing from upstream to downstream in a conveyance direction of a recording medium is generated when the recording medium is conveyed at a position just below the recording head. Accordingly, in a noncontact printing method in which ink droplets **20** are ejected onto a print sheet **10** from a nozzle **121** of an ink head **120**, the ink droplets **20** are drifted to a downstream side in the conveyance direction of the print sheet **10** under the influence of the conveyance airstream W**1**, and attached to the print sheet **10** at positions deviated from their intended trajectory. This is so-called landing deviation, and causes deterioration in image quality.

For example, Patent Document 1 copes with such a problem. In the technique of Patent Document 1, when ink droplets are ejected while a recording medium and an ink head having multiple nozzles are moved relative to each other in a direction crossing a nozzle arrangement direction, the ejection is controlled by increasing the ejection speed for a smaller size of droplets. This suppresses landing deviation of ink droplets attributable to the conveyance airstream.

[Patent Document 1] Japanese Patent Application Publication No. 2010-173178

SUMMARY OF THE INVENTION

In addition to the conveyance airstream W**1**, as shown in FIG. **16**B, an airstream W**2** (hereinafter called a self-produced airstream) flowing from the ink head **120** toward the recording medium is generated at the position right below the ink head **120** when the ink droplets **20** are ejected from the nozzle **121**.

The self-produced airstream W**2** by the ink droplets is generated constantly, for example, when a maximum number of ink droplets are ejected from a nozzle corresponding to pixels present in a solid area. In particular, when the nozzle ejects the maximum number of droplets consecutively to pixels arranged in a sub-scanning direction (sheet conveyance direction), the generation of the self-produced airstream W**2** is remarkably constant. Flowing vertically downward, the self-produced airstream W**2** reduces the influence of the conveyance airstream W**1** and thus reduces the amount of landing deviation of the ink droplets **20**.

On the other hand, in the case of a single-shot ejection where one ink droplet is ejected to every five pixels, for example, the generation of the self-produced airstream W**2** is not constant. As a result, the ejected ink droplet is largely affected by the conveyance airstream W**1** and drifted farther away, increasing the amount of landing deviation.

In this way, the amount of landing deviation by which the ink droplet is drifted by the conveyance airstream W**1** varies depending on a time interval between consecutive ink droplet ejections. Accordingly, using only the technique as disclosed in Patent Document 1 with uniform control to increase the ejection speed for a smaller size of ink droplets cannot resolve the landing deviation of ink droplets and cannot prevent image quality degradation.

The present invention has been made in view of the foregoing points, and aims to provide an image formation apparatus which is capable of improving the landing position accuracy and forming a good image free from landing deviation by resolving the influence of the conveyance airstream and the self-produced airstream which are generated under each ink head when ink droplets are ejected from nozzles onto a recording medium being conveyed.

For the purpose of solving the aforementioned problems, an image formation apparatus of the present invention is an image formation apparatus (for example, an inkjet recording apparatus **100** shown in FIG. **1**) configured to control timing of ink ejection from nozzles (for example, nozzles **121** shown in FIG. **4**) of an ink head (for example, an ink head **120** shown in FIG. **1**), when an image is formed by ejecting ink from each nozzle onto a recording medium (for example, a print sheet **10** shown in FIG. **2**) being conveyed on a conveyance path (for example, a platen belt **160** shown in FIG. **1**), to cope with a conveyance airstream generated by the conveyance of the recording medium. The image formation apparatus is characterized by including an adjustment unit (for example, an ejection control unit **333***b* shown in FIG. **5**) configured to adjust the content of the ejection timing control on the basis of a self-produced airstream rate which is calculated based on a volume of ink ejected from the nozzle per unit time and indicates a generation rate of a self-produced airstream to cause the ink ejected from the nozzle to go straight against the conveyance airstream (for example, an estimated ejection frequency x representing the number of times of ejection of ink from the nozzles per unit time, and a correction coefficient α).

According to the above invention, the conveyance airstream flowing from upstream to downstream in the conveyance direction is generated between the nozzle and the recording medium (conveyance path) in response to the conveyance of the recording medium. In the meantime, as the volume of ink ejected from the nozzle per unit time increases, the self-produced airstream flowing in the ink ejection direction is generated between the nozzle and the recording medium (conveyance path). The degree at which the self-produced airstream causes the ink ejected from the nozzle to go straight against the conveyance airstream increases as the volume of ink ejected from the nozzle per unit time increases. The content of adjustment to the ejection timing control is determined based on the self-produced airstream rate indicating the generation rate of the self-produced airstream, and the content of the ejection timing control is adjusted using the adjustment content thus determined.

Thus, it is possible to adjust the ink ejection timing control on the nozzle while taking into consideration how much the self-produced airstream flowing in the ink ejection direction reduces the landing deviation of ink due to the conveyance airstream in accordance with the generation rate of the self-

produced airstream. Thereby, the landing position accuracy can be improved, and a good image free from landing deviation can be formed.

The image formation apparatus of the present invention is characterized by further including: a storage unit (for example, a storage unit **334** shown in FIG. **5**) configured to store profile data (for example, profile data shown in FIG. **6**) in which the number of ink ejections from the nozzle per unit time is associated with an amount of landing deviation of ink on the recording medium; and a judgment unit (for example, a correction judgment unit **333***c* shown in FIG. **5**) configured to judge whether or not the adjustment to the ejection timing control is needed, on the basis of a result of comparison between the volume of ink ejected from the nozzle per unit time and an ink ejection volume threshold corresponding to the self-produced airstream rate, and is characterized in that, in the case where the judgment unit judges that the adjustment to the ejection timing control on the nozzle is needed, the adjustment unit calculates the number of ink ejections from the nozzle per unit time from the volume of ink ejected from the nozzle per unit time, determines an amount of landing deviation of ink corresponding to the calculated number of ink ejections on the basis of the profile data, and adjusts the content of the ejection timing control using an adjustment content determined based on the self-produced airstream rate corresponding to the determined amount of landing deviation.

According to the above aspect, when the volume of ink ejected from the nozzle per unit time exceeds the ink ejection volume threshold corresponding to the self-produced airstream rate, the number of ink ejections from the nozzle per unit time is calculated from the volume of ink ejected from the nozzle per unit time, and the amount of landing deviation of ink corresponding to the calculated number of ink ejections is obtained from the profile data. Then, the ink ejection timing control on the nozzle to cope with the conveyance airstream is adjusted using the adjustment content corresponding to the amount of landing deviation thus obtained.

Thus, it is possible to adjust the ink ejection timing control on the nozzle while taking into consideration how much the self-produced airstream flowing in the ink ejection direction reduces the landing deviation of ink due to the conveyance airstream in the case where the self-produced airstream is generated constantly. Thereby, the landing position accuracy can be improved and a good image free from landing deviation can be formed.

The image formation apparatus of the present invention is characterized in that the judgment judges: whether or not the nozzle has ejected at least one drop of ink to each of a predetermined number of pixels consecutively located on the recording medium at a position downstream of the nozzle in a conveyance direction of the recording medium, as the result of comparison between the volume of ink ejected for the past predetermined period of time and the threshold; and judges that the adjustment to the ejection timing control on the nozzle is needed if judging that the nozzle has ejected at least one drop of ink to each of the pixels.

According to the above aspect, in the case where at least one drop of ink is ejected to each of the predetermined number of consecutive pixels, the self-produced airstream can be expected to be generated constantly by the consecutive ejection of ink for the predetermined number of pixels. Accordingly, the amount of landing deviation of ink is determined based on an average number of ink ejections calculated from the volume of ink ejected for the past predetermined period of time, and the ejection timing control is adjusted using the adjustment content corresponding to the amount of landing deviation thus determined. Thereby, it is possible to adjust the ink ejection timing control on the nozzle while taking into consideration the amount of change in the amount of landing deviation of ink due to the self-produced airstream.

In addition, the image formation apparatus of the present invention is characterized by further including: a sheet type acquisition unit (for example, a sheet type acquisition unit **335** shown in FIG. **5**) configured to acquire information on a thickness of the recording medium; and a drive control unit (for example, a head gap control unit **332***a* shown in FIG. **5**) configured to change a distance between the conveyance path and an ejection surface of the nozzle on the basis of the information on the thickness acquired by the sheet type acquisition unit, and is characterized in that: the storage unit stores a plurality of the profile data corresponding to the distance between the conveyance path and an ejection surface of the nozzle; and the adjustment unit adjusts the ejection timing control in accordance with the distance changed by the drive control unit.

According to the above invention, even when the clearance between the conveyance belt and the ejection surface of the ink head increases, the adjustment content on the ejection timing control is corrected in accordance with the clearance. Thereby, it is possible to correct the landing position appropriately, and to provide a good image free from landing deviation even when the self-produced airstream changes due to the head gap.

Moreover, the image formation apparatus according to the present invention is characterized by further including a suction unit configured to suck the recording medium to the conveyance path, and is characterized in that, in the case where the nozzle is located in an area within a predetermined distance from any of a leading end (for example, a leading end area A**1** shown in FIG. **12**) and a trailing end (for example, a trailing end area A**2** shown in FIG. **12**) of the recording medium, the adjustment unit adjusts the ejection timing control in accordance with an airstream caused by the suction unit.

According to the above invention, in the leading end and the trailing end of the print sheet where the landing deviation is likely to be influenced by the airstream caused by the suction unit, the ejection timing control can be adjusted in accordance with the airstream. Thereby, the landing position accuracy can be improved and a good image free from landing deviation can be provided.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. **1** is a schematic cross-sectional diagram showing an internal configuration of an inkjet recording apparatus according to a first embodiment of the present invention.

FIG. **2** is an explanation diagram showing, from a lateral side, an image formation path of FIG. **1** along which an image is formed.

FIG. **3**A is an explanation diagram showing a head holder, which is placed above a conveyance path in the inkjet recording apparatus of FIG. **1**, as viewed from below.

FIG. **3**B is an explanation diagram showing, in a magnified manner, a side cross section of the head holder which is placed above the conveyance path in the inkjet recording apparatus of FIG. **1**.

FIG. **4** is a magnified side view of a part of the image formation path of FIG. **1**.

FIG. **5** is a block diagram showing functional modules of a processing unit of FIG. **1** which relate to an ejection timing correction function.

FIG. **6** is an explanation diagram showing profile data on the amount of landing deviation with respect to the ink ejection frequency stored in a storage unit of FIG. **5**.

FIG. **7**A is a graph showing the relationship between the ink ejection frequency and the amount of landing deviation in the profile data of FIG. **6**, and is a graph showing the case where the head gap is 1.6 mm.

FIG. **7**B is a graph showing the relationship between the ink ejection frequency and the amount of landing deviation in the profile data of FIG. **6**, and is a graph showing the case where the head gap is 3.0 mm.

FIG. **8** is a top view for explaining a unit line to be selected by the processing unit of FIG. **1**.

FIG. **9** is a flowchart briefly showing an ejection timing correction operation in the inkjet recording apparatus of FIG. **1**.

FIG. **10** is a side view showing a suction airstream generated right below an ink head of an inkjet recording apparatus according to a second embodiment.

FIG. **11**A is a side view showing the condition of the suction airstream generated depending on the conveyance position of a print sheet in FIG. **10**, and showing the case where the leading end of the print sheet is located right below a nozzle.

FIG. **11**B is a side view showing the condition of the suction airstream generated depending on the conveyance position of the print sheet in FIG. **10**, and showing the case where a central portion of the print sheet is located right below the nozzle.

FIG. **11**C is a side view showing the condition of the suction airstream generated depending on the conveyance position of the print sheet in FIG. **10**, and showing the case where the trailing end of the print sheet is located right below the nozzle.

FIG. **12** is a top view showing a leading end area and a trailing end area of the print sheet which are judged by the processing unit of FIG. **1**.

FIG. **13**A is an explanation diagram showing the positional relationship between the ink head and the print sheet in the case where the suction airstream is generated right below the ink head.

FIG. **13**B is an explanation diagram showing the positional relationship between the ink head and the print sheet in the case where no suction airstream is generated right below the ink head.

FIG. **14** is a graph showing a variation in the amount of landing deviation depending on a distance between an end portion of a print sheet and a position right below a nozzle in the profile data stored in the storage unit of FIG. **5**.

FIG. **15**A is an explanation diagram showing trajectories of ink droplets from the nozzle of FIG. **10** before and after the correction to the ejection timing, in the case where the leading end area of a print sheet is located right below the nozzle.

FIG. **15**B is an explanation diagram showing trajectories of ink droplets from the nozzle of FIG. **10** before and after the correction to the ejection timing, in the case where the trailing end area of the print sheet is located right below the nozzle.

FIG. **16**A is an explanation diagram showing a conveyance airstream generated when a print sheet is conveyed.

FIG. **16**B is an explanation diagram showing a self-produced airstream generated when ink droplets are ejected from a nozzle.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

(First Embodiment)

Embodiments of an image formation apparatus according to the present invention are described in detail below with reference to the drawings.

(Overall Configuration of Inkjet Recording Apparatus)

An embodiment of the present invention is described with reference to the drawings. FIG. **1** is a schematic cross-sectional diagram showing an internal configuration of an inkjet recording apparatus according to a first embodiment of the present invention. FIG. **2** is an explanation diagram showing, from a lateral side, an image formation path along which an image is formed. FIG. **3**A is an explanation diagram showing a head holder, which is placed above a conveyance path in the inkjet recording apparatus of FIG. **1**, as viewed from below. FIG. **3**B is an explanation diagram showing, in a magnified manner, a side cross section of the head holder. FIG. **4** is a magnified side view of a part of the image formation path of FIG. **1**.

Note that the inkjet recording apparatus of the embodiment is an inkjet-type line color printer configured to perform printing on a per-line basis by ejecting either black or colored ink from nozzles of ink heads included in a head unit serving as an image formation unit.

As shown in FIG. **1**, an inkjet recording apparatus **100** is a printing machine configured to eject ink onto and thereby form an image on a print sheet **10** being conveyed along a conveyance path. In this embodiment, the inkjet recording apparatus **100** is an inkjet-type line color printer including: a paper feed unit configured to feed a print sheet **10**; a sheet conveyance unit (including a platen belt **160**) configured to convey the print sheet **10**; a sheet discharge port **150** as a sheet discharge unit configured to discharge a printed print sheet **10**; and the like.

The inkjet recording apparatus **100** includes multiple ink heads **120** as a printing mechanism, which extends in a direction orthogonal to a sheet conveyance direction and has multiple nozzles formed therein, and forms an image on a per-line basis by ejecting either black or colored ink from a nozzle **121** of each ink head **120**.

The inkjet recording apparatus **100** also includes: a processing unit **330** formed of, for example, a controller board on which a CPU, a memory, and the like are placed; a manipulation panel which displays a menu and accepts manipulation by the user, for example; and other function units (not illustrated).

Print sheets are fed one by one from the paper feed unit such as a side paper feed tray or a front paper feed tray, conveyed along a paper-feed-system conveyance path inside a chassis by drive mechanisms such as a roller, and guided to register rollers **240**. Here, the register rollers **240** are a pair of rollers provided to align leading edges of and correct skew orientation of a print sheet. A fed print sheet is suspended by the register rollers **240**, and conveyed toward a head unit **110** at predetermined timing.

As shown in FIG. **2**, an image formation path CR**1** is provided downstream of the register rollers **240** in the conveyance direction.

The inkjet recording apparatus **100** of the embodiment includes the image formation path CR**1** as its conveyance path. The print sheet **10** is conveyed on the platen belt **160** along the image formation path CR**1** at a speed determined depending on print conditions. Above the image formation path CR**1**, the head unit **110** is placed opposed to the platen belt **160**. The nozzles of the ink heads **120** included in the

head unit **110** eject ink of multiple colors onto the print sheet **10** on the platen belt **160** on a per-line basis, so that multiple images are formed thereon to overlap one another.

More specifically, the image formation path CR**1** includes: the platen belt **160** which is an endless conveyer belt; and a drive roller **161** and a driven roller **162** which are drive mechanisms of the platen belt **160**; and the like. A head holder **500** holding the ink heads **120** is provided above the image formation path CR**1**.

The head holder **500** is a box having a head holder surface **500***a* as its bottom surface. The head holder **500** is configured to hold and fix the ink heads **120** therein as well as house, as a unit, other function parts for ejecting ink from the ink heads **120**. Moreover, the head holder surface **500***a* being the bottom surface of the head holder **500** is placed opposed to and parallel to the conveyance path. Multiple attachment openings **500***b* having the same shapes as horizontal cross sections of the respective multiple ink heads **120** constituting the head unit **110** are arranged in the head holder surface **500***a*. The ink heads **120** are inserted into the respective attachment openings **500***b* while their discharge ports protrude from the head holder surface **500***a*.

The image formation path CR**1** also includes a mechanism for changing a distance (head gap) between an ejection surface of each ink head **120** and the platen belt **160** in order to prevent the print sheet **10** from hitting against the ink heads **120**. This mechanism is configured to change the distance between the ejection surfaces of the ink heads **120** and the platen belt **160** by moving the platen belt **160** vertically with respect to the ink heads **120**.

As shown in FIG. **3**A, the ink heads **120** are arranged in rows in a direction (main-scanning direction) orthogonal to the conveyance direction (sub-scanning direction). The ink heads **120** in each of the rows are staggered so as not to overlap the ink heads **120** of the adjacent rows in the conveyance direction. The rows of the ink heads **120** are arranged at predetermined intervals in the conveyance direction, and a main-scanning flow path **111** is formed between every two adjacent rows. The ink heads **120** adjacent in each row are arranged at predetermined intervals, and a sub-scanning flow path **112** is formed between every two adjacent ink heads **120**, **120**. The main-scanning flow paths **111** and the sub-scanning flow paths **112** communicate with one another to form a mist discharge path in the form of mesh.

Each main-scanning flow path **111** is provided with a stepped guide roller **510**. The stepped guide roller **510** is formed by coupling guide rollers of different diameters together into one roller, and is formed by carving a metal rod, for example. More specifically, the stepped guide roller **510** has such a configuration that upstream guide rollers **510***a* having a large diameter and downstream guide rollers **510***b* having a diameter smaller than those of the upstream guide rollers **510***a* are alternately arranged and coupled together on a single rotational axis.

Each upstream guide roller **510***a* is provided upstream of the corresponding ink head **120** in the conveyance direction, and is rotated by being biased downward and pressed against an upper surface of the conveyance path. On the other hand, each downstream guide roller **510***b* is provided downstream of the corresponding ink head **120** in the conveyance direction, and is rotatably supported at a position away from the upper surface of the conveyance path by a predetermined distance.

The upstream guide rollers **510***a* and the downstream guide rollers **510***b* are also staggered to correspond to the staggered arrangement of the ink heads **120**. Moreover, because the stepped guide rollers **510** are arranged in the main-scanning flow paths **111**, the upstream guide rollers **510***a* and the downstream guide rollers **510***b* are also arranged in the main-scanning flow paths **111** alternately.

Meanwhile, the platen belt **160** is an endless belt member configured to convey a recording medium. As shown in FIG. **2**, the platen belt **160** circles by means of the drive roller **161** and slides in an area opposed to the ink heads **120** to convey the print sheet **10**. More specifically, the platen belt **160** is wound around the pair of the drive roller **161** and the driven roller **162** which are arranged orthogonal to the conveyance direction in which the print sheet **10** is conveyed, and circles in the conveyance direction by means of the drive force of the drive roller **161**.

Moreover, as shown in FIG. **4**, the platen belt **160** has many belt holes **165** for adsorbing a print sheet **10**, and a platen plate **620** is placed below the platen belt **160**. The platen plate **620** is a plate-shaped member configured to slidably support the platen belt **160** at a position opposed to the ink heads **120** and having many suction holes **622** made by penetrating the platen plate **620** at locations where the belt holes **165** pass. A suction fan **650** serving as a suction unit is provided below the platen plate **620**.

The suction fan **650** is the suction unit configured to generate a negative pressure for adsorbing a print sheet **10** located on the upper surface of the platen belt through the suction holes and the belt holes **165**. The negative pressure generated by the suction fan **650** adsorbs the print sheet **10** on the platen belt **160**. Further, the negative pressure generated by the suction fan **650** generates an airstream which flows downward after passing through the belt holes **165** of the platen belt **160** and the suction holes **622** of the platen plate **620**.

The print sheet **10** is conveyed along the image formation path CR**1** having the above configuration, by the annular platen belt **160** provided opposed to the ink heads **120**, at a speed according to the print conditions. While the sheet is conveyed on this path, an image is formed thereon on a per-line basis by ink ejected by each of the ink heads **120**.

The ink heads **120** are configured to eject ink of four colors: K (black); C (cyan); M (magenta); and Y (yellow). On a bottom surface of each ink head **120**, multiple nozzles **121** for ejecting ink are arranged in the main-scanning direction.

Ink droplets are ejected from the nozzles **121** by a predetermined volume (drop volume) for each pixel, whereby an image subjected to gradation processing is formed. Specifically, ink is ejected to each pixel in units of drops from the nozzles **121** in accordance with a drive signal transmitted from the processing unit **330**. The density of each color is changed by the number of droplets of ink ejected (the number of drops), and the volume of each droplet is adjusted as a drop size. In this event, a conveyance airstream flowing from upstream to downstream in the conveyance direction is generated when the print sheet **10** is conveyed to a position right below the ink head. Moreover, a self-produced airstream flowing from the ink head **120** toward the print sheet **10** is generated constantly because the ink droplets **20** are continuously ejected from the nozzles **121**.

The processing unit **330** is a computing module formed of: hardware including a processor such as a CPU or DSP (Digital Signal Processor), a memory, and other electronic circuits; software including programs having the function of such hardware; or a combination of these. The processing unit **330** is configured to virtually build various functional modules by loading and executing programs as appropriate, and to perform processing related to image data, control over operations of the respective parts, and various kinds of processing in response to the user's manipulation by use of the functional modules thus built. In particular, in the embodiment, the

processing unit **330** has a function of correcting ink ejection timing in order to correct the landing deviation caused on the image formation path CR**1** by the conveyance airstream and the self-produced airstream.

(Internal Configuration of Processing Unit **330**)

The ink ejection timing correcting function described above is implemented by causing the processing unit **330** of the inkjet recording apparatus **100** to control operations of the head unit **110** and the other drive units.

FIG. **5** is a block diagram showing ejection timing-related functional modules in the processing unit **330**. FIG. **6** is an explanation diagram showing profile data on the amount of landing deviation with respect to the ink ejection frequency stored in a storage unit **334**. FIGS. **7**A and **7**B are graphs showing the relationship between the ink ejection frequency and the amount of landing deviation in the profile data of FIG. **6**. FIG. **7**A corresponds to the case where the head gap is 1.6 mm, whereas FIG. **7**B corresponds to the case where the head gap is 3.0 mm. FIG. **8** is a top view for explaining a unit line selected by the processing unit **330**.

Note that a "module" used in the description indicates a function unit for implementing a certain operation and is formed of: hardware such as a device or an instrument; software having the function of such hardware; or a combination of these.

As shown in FIG. **5**, the processing unit **330** mainly includes: a job data reception unit **331**; an image processing unit **333**; a drive control unit **332**; the storage unit **334**; a manipulation signal acquisition unit **336**; and a sheet type acquisition unit **335**.

The job data reception unit **331** is a communication interface configured to receive job data being units of a series of print processing, and is a module configured to give the print data included in the received job data to the image processing unit **333**. The communication mentioned here includes, for example, LANs including an intranet (intra-company network) and a home network via a 10BASE-T, 100BASE-TX, or the like, as well as short-distance communication such as infrared communication.

The manipulation signal acquisition unit **336** is a module configured to receive a manipulation signal inputted by the user through a manipulation panel **361**, and is configured to analyze the received manipulation signal and make another module execute processing in response to the user's manipulation. In particular, in the embodiment, the manipulation signal acquisition unit **336** is configured to accept instruction manipulation on drop volume correction processing and print setting information such as the type of the print sheet **10**, from the manipulation panel **361**, a printer driver connected thereto through external communication, or the like.

The sheet type acquisition unit **335** is a module configured to acquire sheet type data on paper feed, such as the size, type, or thickness of the print sheet **10**, detected by the job data reception unit **331** and the manipulation signal acquisition unit **336**. At the time of print processing, the sheet type acquisition unit **335** transmits the acquired sheet type data to the drive control unit **332** and the image processing unit **333**.

The storage unit **334** is a memory device or the like configured to store and hold various kinds of data and programs on image processing. The data stored and held in the storage unit **334** includes: information on a conveyance speed at which to convey a print sheet; and head gap setting information which is information defined based on information on the thickness of the print sheet **10** and related to a distance between the platen belt **160** and the ejection surface of each ink head **120**.

As shown in FIG. **6**, the data stored and held in the storage unit **334** also includes profile data in which a distance between a theoretical ejection landing position and an actual ejection landing position is defined as the amount of landing deviation in association with each ejection frequency. In the profile data, the amount of landing deviation in association with each ejection frequency is stated for each head gap distance, i.e., for each distance between the platen belt **160** and the ejection surface of each ink head **120**.

By using FIGS. **7**A and **7**B, a description is given of the relationship between the ejection frequency and whether a self-produced airstream W**2** is generated at the head gap, and the amount of landing deviation caused by the conveyance airstream W**1** and the self-produced airstream W**2**. In FIGS. **7**A and **7**B, the horizontal axis indicates the ejection frequency (unit: [Hz]) which denotes the average number of times of ejection of ink droplets per unit time, and the vertical axis indicates the amount of landing deviation (unit: [μm]).

The ejection frequency is defined as the number of times each nozzle **121** ejects ink droplets **20** per unit time. The ejection time interval is long at an ejection frequency of 1 Hz, and becomes shorter as the ejection frequency comes closer to 150 KHz. As shown in FIGS. **7**A and **7**B, ink ejection at an ejection frequency of 1 Hz generates no self-produced airstream W**2** from the nozzle **121**, and therefore exhibits a large amount of landing deviation attributable to the influence of only the conveyance airstream W**1**. On the other hand, as the ejection frequency gets closer to 150 KHz, the influence of the self-produced airstream W**2** becomes larger, and hence the amount of landing deviation becomes smaller.

Note that, in the embodiment, the ejection frequency of 1 Hz is defined as a frequency calculated when a total volume of ink ejected per 30 dots is less than 1 drop. The ejection frequency of 150 KHz indicates a frequency calculated when a total volume of ink ejected per 30 dots is equal to the maximum ink volume. Here, the maximum ink volume denotes the volume of ink ejected in the case where seven drops are ejected to each of 30 dots using a multidrop technique.

Hereinbelow, the maximum number of times each nozzle **121** is capable of ejecting ink droplets **20** per unit time is defined as a maximum ejection frequency MD (unit: [Hz]). In the embodiment, the maximum ejection frequency MD is equal to the ejection frequency of 150 KHz.

The profile data may be set individually for each inkjet recording apparatus **100** while an individual difference among inkjet recording apparatuses **100** is taken into consideration. Information on the individual difference includes, for example, information on a change in each of the airstreams depending on information on: a distance (head gap) between the ejection surface of each ink head **120** and the platen belt **160**; and meandering of the platen belt **160** for conveying the print sheet **10**. Further, although the profile data is acquired at the time of factory shipment in the embodiment, the acquisition timing is not limited to the timing of factory shipment. Instead, the profile data may be acquired at the time of print start, environmental change, temporal change, or maintenance.

The drive control unit **332** is a module configured to control the operations of the respective functions in the inkjet recording apparatus **100** such as a drive unit **350** configured to drive the parts on the conveyance path. In the embodiment, the drive control unit **332** includes a head gap control unit **332***a*.

The head gap control unit **332***a* is a module configured to control a head gap adjustment unit **350***a* by referring to head gap setting information stored in the storage unit **334** on the basis of information on the thickness of the print sheet **10**

acquired from a print job, in such a way that a clearance (head gap) between each ink head **120** and the platen belt **160** depending on the thickness of the print sheet **10** becomes equal to a predetermined distance.

The head gap adjustment unit **350***a* is a mechanism configured to change the distance between each ink head **120** and the platen belt **160** in order to prevent the print sheet **10** from hitting against the ink head **120**. The head gap adjustment unit **350***a* changes the distance between the ink head **120** and the platen belt **160** by, for example, causing the drive mechanism controlled by electrical signals to move the platen belt **160** vertically with respect to the ink head **120**. Alternatively, the ink head **120** may be moved with respect to the platen belt **160**.

The image processing unit **333** is a processor configured to perform digital signal processing specialized for image processing, and is a module configured to perform conversion on image data and the like necessary for printing and execute the printing. The image processing unit **333** includes an ejection control unit **333***b* and a color conversion circuit **333***a*.

The color conversion circuit **333***a* is a module configured to convert a RGB print image being acquired image data into a CMYK print image. In the embodiment, the color conversion circuit **333***a* subjects the image data to halftone processing to convert it into image data related to the volume of drops of the ink heads **120**.

The ejection control unit **333***b* is a module configured to control ejection from the nozzles **121** for ejecting ink onto the print sheet **10**. The ejection control unit **333***b* calculates the volume of ink to be ejected to each dot on the basis of the image data subjected to the image processing, and ejects ink drops, the number of which is determined based on the gradations of the image data, for each dot at predetermined timing. In the embodiment, the ejection control unit **333***b* is set in advance to eject ink at the corrected ejection timing obtained by correcting the regular timing, in order to eliminate the amount of landing deviation caused by the conveyance airstream W**1**. The amount of correction to the ejection timing (default correction amount) may be changed by a re-correction instruction made by a correction judgment unit **333***c*.

In addition, the image processing unit **333** includes the correction judgment unit **333***c* and a correction time calculation unit **333***d* as functions to determine how much to change the default correction amount in accordance with the amount by which the amount of landing deviation caused by the conveyance airstream W**1** is changed by the generation of the self-produced airstream W**2**, the default correction amount being used when the ejection control unit **333***b* corrects the ejection timing.

The correction judgment unit **333***c* is a module configured to judge whether or not the self-produced airstream W**2** will be generated constantly when ink is ejected from a certain nozzle **121**. In the embodiment, the correction judgment unit **333***c* judges whether or not the self-produced airstream W**2** will be generated constantly by referring to a history of ejection from the nozzle **121** in a certain area including multiple pixels and comparing it with a predetermined threshold.

More specifically, as shown in FIG. **8**, the correction judgment unit **333***c* selects, as a unit line D**1**, a certain area covering **30** dots which are continuously arranged downstream in the conveyance direction of a certain nozzle E**1** for ejecting ink. Then, the correction judgment unit **333***c* multiplies the volume of each ink droplet by the number of drops for each dot in the unit line D**1** to obtain a total volume of ink ejected in the unit line D**1**. Meanwhile, a volume of ink per unit line D**1**, with which a self-produced airstream W**2** would be generated constantly, is set as the threshold.

Then, if the total volume of ejected ink is equal to or smaller than the predetermined threshold, the correction judgment unit **333***c* judges that no self-produced airstream W**2** will be generated constantly, and sends the ejection control unit **333***b* this judgment result as a re-correction instruction that no change needs to be made on the default correction amount. On the other hand, if the total volume of ejected ink is equal to or larger than the predetermined threshold, the correction judgment unit **333***c* judges that a self-produced airstream W**2** will be generated constantly, and sends the judgment result to the correction time calculation unit **333***d*.

Note that, in the embodiment, the correction judgment unit **333***c* compares the total volume of ink ejected per unit line D**1** with the threshold; however, the correction judgment unit **333***c* may further judge whether or not one or more ink droplets are ejected to every dot in the unit line D**1**. In this case, the correction judgment unit **333***c* judges that the self-produced airstream W**2** will be generated constantly if one or more ink droplets are ejected continuously.

In short, the threshold which is used for the correction judgment unit **333***c* to judge whether the self-produced airstream W**2** will be generated constantly can be set in the form of parameters, such as the volume of ejected ink and the number of ink droplets for each dot, which reflect the situation where the self-produced airstream W**2** is generated constantly. These are parameters for estimating the self-produced airstream rate as the generation rate of the self-produced airstream.

The correction time calculation unit **333***d* is a module configured to calculate the amount of correction time, by which the ejection timing is to be adjusted, by calculating the amount of landing deviation due to the conveyance airstream W**1** and the self-produced airstream W**2** on the basis of the total volume of ejected ink, in response to the judgment result from the correction judgment unit **333***c* that there is a self-produced airstream W**2**.

Specifically, while taking into consideration the fact that the amount of landing deviation due to the conveyance airstream W**1** varies depending on the influence of the self-produced airstream W**2**, the correction time calculation unit **333***d* calculates, as a correction time Δt (unit: [μs]), the amount of change to be made to the default correction amount, which the ejection control unit **333***b* uses for the ejection timing correction, in accordance with the amount of variation in the amount of landing deviation, if the correction judgment unit **333***c* judges that there is a self-produced airstream W**2**. More specifically, the correction time calculation unit **333***d* calculates the difference between the amount of landing deviation caused when only the conveyance airstream W**1** is generated and the amount of landing deviation caused when both the conveyance airstream W**1** and the self-produced airstream W**2** are generated and, from this difference, calculates the correction time Δt which is the amount of change to be made to the default correction amount.

Here, the amount of landing deviation caused when only the conveyance airstream W**1** is generated is the amount of landing deviation caused in a condition where there is no influence of the self-produced airstream W**2**. Hence, this amount is equal to the amount of landing deviation f(1) at an ejection frequency of 1 Hz whose ejection time interval is long as shown in FIGS. **7**A and **7**B.

On the other hand, when both the conveyance airstream W**1** and the self-produced airstream W**2** are generated, the landing position of ink gets closer to a point without landing deviation since the ink is drifted back to the upstream side in

the conveyance direction under the influence of the self-produced airstream W**2**. Hence, as shown in FIGS. **7**A and **7**B, the amount of landing deviation caused in this case is equal to the amount of landing deviation (f(x)) at an ejection frequency of any of 1 Hz to 150 KHz.

Thus, a correction time Δt**1** obtained by the following equation (EQ1) is set as the correction time **66** t:

$$\Delta t1=(f(1)-f(x))/v \quad \text{(EQ1)}$$

where f(1) indicates the amount of landing deviation (unit: [μm]) at an ejection frequency of 1 Hz, f(x) indicates the amount of landing deviation (unit: [μm]) at an estimated ejection frequency x (unit: [Hz]), and v indicates a conveyance speed (unit: [μm/μs]) of the platen belt **160**.

The correction time calculation unit **333***d* needs to obtain the estimated ejection frequency x for the purpose of calculating the amount of landing deviation f(x) including the influence of the self-produced airstream W**2**. To this end, in the embodiment, the estimated ejection frequency x is obtained by: calculating a correction coefficient α, which indicates how much the self-produced airstream W**2** affects the landing position of ink droplets **20**, from the ratio of the number of dots and the number of times of ink ejection in the unit line D**1** to the maximum number of dots and the maximum number of times of ink ejection in the unit line D**1**; and multiplying the correction coefficient α by the ejection frequency of 150 KHz which is the maximum ejection frequency MD.

Specifically, the correction coefficient α is obtained by the following mathematical formula:

(correction coefficient α)=(correction coefficient α in unit line *D*1)=(number of ejected dots/total number of dots in unit line *D*1)×(average number of drops for each dot/maximum number of drops ejected to each dot)

where (average number of drops for each dot)=(total number of ejected drops/number of ejected dots).

The estimated ejection frequency x is obtained by the following mathematical formula:

(estimated ejection frequency *x*)=(correction coefficient α)×(maximum ejection frequency MD)

Then, the correction time Δt is calculated using the estimated ejection frequency x obtained from the correction coefficient α. Now, a description is given of how to calculate the correction time Δt. Here, the case where the conveyance speed of the platen belt **160** is 0.632 μm/μs and the head gap is 3.0 mm is described.

In a case where the history of ejection in the unit line D**1** shows that a maximum of 7 drops are ejected to each of 30 dots, for example, the correction coefficient α is obtained as follows:

(correction coefficient α)=(30 dots/30 dots)×(7 drops/7 drops)=1

Meanwhile, in the case where the history of ejection in the unit line D**1** shows a maximum of 7 drops are ejected to each of 15 dots, for example, the correction coefficient α is obtained as follows:

(correction coefficient α)=(15 dots/30 dots)×(7 drops/7 drops)=0.5

When the correction coefficient α is 1, the estimated ejection frequency x is equal to 150 KHz because the maximum ejection frequency MD is 150 KHz in the embodiment. When the estimated ejection frequency x is the ejection frequency of 150 KHz, the amount of landing deviation f(150000) is 87.69 μm as shown in FIG. **6**. Accordingly, the correction time Δt in this case is as follows:

$$\Delta t=(98.91-87.69)/0.632=17.75\ [\mu s].$$

When the estimated ejection frequency x is the ejection frequency of 100 Hz, the amount of landing deviation f(100) is 89.96 μm as shown in FIG. **6**. Accordingly, the correction time Δt in this case is as follows:

$$\Delta t=(98.91-89.96)/0.632=14.16\ [\mu s].$$

As described above, correction data on the correction time Δt calculated from the correction coefficient α and the estimated ejection frequency x is transmitted to the ejection control unit **333***b*. Based on the correction data, the ejection control unit **333***b* corrects the drive signal in such a way that the ejection timing is moved forward by the correction time Δt so that ink may land at the same position as the landing position obtained by correcting the amount of landing deviation which would be caused by the conveyance airstream W**1** in the case of a single-shot ejection of the ink. Then, the ejection control unit **333***b* inputs the corrected signal into the ink heads **120**. For example, when the correction coefficient is 1, the ejection control unit **333***b* performs control such that the ejection timing becomes earlier by 17.75 μs than the ejection timing corresponding to the conveyance airstream W**1**.

To put it simply, the ejection control unit **333***b* changes (adjusts) the default amount of correction to the ejection timing, which is determined depending on the amount of landing deviation due to the conveyance airstream W**1**, by use of the correction time Δt in accordance with the self-produced airstream rate corresponding to the amount of change in the amount of landing deviation caused by the self-produced airstream W**2**.

(Ejection Timing Correction Operation)

Next, a description is given of an ejection timing correction operation in the inkjet recording apparatus **100** having the above configuration. FIG. **9** is a flowchart showing the ejection timing correction operation in the inkjet recording apparatus **100**.

As shown in FIG. **9**, first of all, the job data reception unit **331** receives job data (Step S**101**), and transmits the job data to the image processing unit **333** and the sheet type acquisition unit **335**. The sheet type acquisition unit **335** acquires sheet thickness information from the type of a print sheet **10** included in the job data, and inputs the thickness information into the drive control unit **332** and the image processing unit **333**. The head gap control unit **332***a* of the drive control unit **332** having acquired the thickness information determines the distance between the platen belt **160** and the ejection surface of each ink head **120** with reference to the head gap setting information in the storage unit **334**, and drives and controls the head gap adjustment unit **350***a*.

Meanwhile, the image processing unit **333** acquires information on the distance (head gap) between the platen belt **160** and the ejection surface of each ink head **120** stored in the storage unit **334**, on the basis of the sheet type information. From the storage unit **334**, the image processing unit **333** also acquires setting information on the conveyance speed of the platen belt **160** (Step S**102**).

Upon receiving the job data, the image processing unit **333** first causes the color conversion circuit **333***a* to subject image data in the job data to halftone processing to create image data on the number of drops to be ejected from each nozzle **121** for

each dot and the volume of each drop, and inputs the image data into the correction judgment unit **333***c* and the ejection control unit **333***b*.

The ejection control unit **333***b* ejects ink onto the print sheet **10** sequentially from a leading end portion of the sheet in the conveyance direction, on the basis of the image data calculated by the color conversion circuit **333***a*. In this event, the ejection control unit **333***b* determines whether or not to perform adjustment (correction) to cancel the ejection timing control for eliminating the landing deviation due to the influence of the conveyance airstream W**1** by the amount equivalent to the amount of change in the landing position due to the influence of the self-produced airstream W**2**, on the basis of the result of judgment on whether or not a self-produced airstream W**2** is generated from each nozzle constantly, the judgment result being transmitted from the correction judgment unit **333***c*.

More specifically, the correction judgment unit **333***c* selects, as a unit line (predetermined area) D**1**, 30 dots which are arranged downstream of a certain nozzle E**1** for ejecting ink in the conveyance direction. Then, referring to the history of ejection in the unit line D**1**, the correction judgment unit **333***c* calculates a total volume of ejected ink from the volume of each ink droplet, the number of drops ejected to each dot, and the number of dots (30 dots) (Step S**104**). The correction judgment unit **333***c* also judges whether or not the total volume of ejected ink, thus obtained, is equal to or larger than the predetermined threshold (Step S**105**).

If the total volume of ejected ink is not equal to or larger than the predetermine threshold (if NO in step S**105**), the correction judgment unit **333***c* judges that no self-produced airstream W**2** will be generated constantly, and sends the ejection control unit **333***b* this judgment result as a re-correction instruction that no change needs to be made to the default correction amount (Step S**109**). Here, when ink is ejected for the first time, for example, a total volume of ejection is zero because no ejection history exists. Accordingly, it is judged that no self-produced airstream W**2** will be generated constantly and, in response to this judgment result, the ejection control unit **333***b* ejects ink from each nozzle **121** at the previously defined ejection timing corresponding to the amount of landing deviation due to the conveyance airstream W**1** (the ejection timing obtained by correcting the regular ejection timing by means of the default correction amount) (Step S**110**). Note that ejection history information made at this time is transmitted to the correction judgment unit **333***c*.

On the other hand, if the total volume of ejected ink is equal to or larger than the predetermined threshold (if YES in Step S**105**), the correction judgment unit **333***c* judges that the self-produced airstream W**2** will be generated constantly, and transmits this judgment result to the correction time calculation unit **333***d*.

Upon acquisition, from the correction judgment unit **333***c*, of the judgment result that the self-produced airstream W**2** will exist, the correction time calculation unit **333***d* first calculates the correction coefficient α from the history of ejection in the unit line D**1**, i.e., 30 dots (Step S**106**). Then, the correction time calculation unit **333***d* obtains an estimated ejection frequency x by multiplying the correction coefficient a by the ejection frequency of 150 KHz which is the maximum ejection frequency MD.

After that, while referring to the profile data in FIG. **6**, on the basis of the estimated ejection frequency x (Step S**107**), the correction time calculation unit **333***d* calculates the amount of landing deviation f(x) including the influence of the self-produced airstream W**2**, which will occur in the next ink ejection.

Subsequently, based on the calculated amount of landing deviation f(x), the correction time calculation unit **333***d* calculates the correction time Δt as correction data from the above equation (EQ1) (Step S**108**). The correction data on the correction time Δt thus calculated is inputted into the ejection control unit **333***b*.

The ejection control unit **333***b* changes (adjusts) the default correction amount on the basis of the correction data, corrects the ejection timing using the default correction amount changed in such a way that the ejection timing becomes earlier than the timing before the change, and causes each nozzle **121** to eject ink at the corrected timing (Step S**110**). Thus, even when the self-produced airstream W**2** is generated constantly, the ink lands at the same position as the position at which the ink would land if the ejection timing is corrected by using the default correction amount in the absence of the constant self-produced airstream W**2**.

The ink head **120** ejects ink from all of its nozzles **121** at the ejection timing corresponding to the amount of landing deviation due to the conveyance airstream W**1** (Step S**112**). After that, the ink head **120** judges whether or not ink is to be ejected to the next dot with reference to the job data (Step S**113**). If ink is to be ejected to the next dot (if YES in Step S**114**), the processes from Step S**103** to Step S**112** are executed. On the other hand, if ink is not to be ejected to the next dot (if NO in Step S**114**), the process is terminated.

(Operation and Effect)

According to the embodiment described above, whether or not the self-produced airstream W**2** will be generated constantly at the time of the next ejection of ink from a certain nozzle is judged by use of the threshold with reference to the history of ejection from the nozzle **121**. In addition, according to the embodiment, if the self-produced airstream W**2** will be generated constantly, the ejection frequency which causes the self-produced airstream W**2** is obtained from the ink volume in the ejection history, and the correction is made such that the ejection timing is moved forward based on the amount of landing deviation associated with the ejection frequency thus obtained. This makes it possible to correct the ejection timing while taking into consideration not only the influence of the conveyance airstream W**1** but also the influence of the self-produced airstream W**2**, and thereby to make ink land at an appropriate position in various ejection patterns including patterns accompanied by the self-produced airstream W**2**. In this way, according to the embodiment, even in the case where the self-produced airstream W**2** is generated constantly, the ink landing position can be corrected to the right position as in the case where no self-produced airstream W**2** is generated constantly, whereby a good image free from landing deviation can be provided.

Further, according to the embodiment, the correction judgment unit **333***c* judges whether or not the self-produced airstream W**2** will be generated constantly by judging whether or not at least one ink droplet is ejected to each of **30** dots in the unit line D**1** consecutively. Thereby, the self-produced airstream W**2** caused by ejecting ink for the multiple pixels consecutively can be judged appropriately.

Furthermore, according to the embodiment, the ejection timing is corrected and controlled by calculating the correction time Δt which varies depending on the head gap and the conveyance speed. This makes it possible to appropriately resolve a variation in the landing position, which varies depending on the type of the print sheet **10** and the conveyance speed, to improve the landing position accuracy, and thereby to provide a good image free from landing deviation.

(Second Embodiment)

Next, a second embodiment of the present invention is described. In the embodiment, in addition to the function described above, a description is given of a function of correcting the ejection timing to cope with an airstream caused by suction made by the suction fan **650**.

FIG. **10** is an explanation diagram showing an airstream caused by suction, which is generated right below an ink head **120** of an inkjet recording apparatus according to the second embodiment. FIGS. **11**A to **11**C are explanation diagrams showing, from the lateral side, the condition of the airstream caused by suction, which is generated depending on the conveyance position of a print sheet **10**. FIG. **11**A shows the case where the leading end of the print sheet **10** is located right below a nozzle **121** of the ink head **120**, FIG. **11**B shows the case where a central portion of the print sheet **10** is located right below the nozzle **121**, and FIG. **11**C shows the case where the trailing end of the print sheet **10** is located right below the nozzle **121**. FIG. **12** is a top view showing a leading end area A**1** and a trailing end area A**2** of the print sheet. FIGS. **13**A and **13**B are explanatory diagrams respectively showing the positional relationship between the ink head **120** and the print sheet **10** in the case where the airstream caused by suction is generated right below the ink head **120**, and in the case where no such airstream is generated.

In the embodiment, the suction fan **650** serving as the suction unit is provided below the platen belt **160**, as described above. As shown in FIG. **10**, the negative pressure generated by the suction fan **650** generates an airstream which flows downward after passing through the belt holes **165** of the platen belt **160** and the suction holes **622** of the platen plate **620**.

Here, the belt holes **165** of the platen belt **160** are closed depending on the position of the print sheet **10** being conveyed. Accordingly, in the case where the central portion of the print sheet **10** is located right below the nozzle **121** as shown in FIG. **11**B, for example, no airstream to pass through the belt holes **165** is generated, and therefore ejected ink droplets **20** are affected only by the conveyance airstream W**1**.

On the other hand, in the case where the leading end or trailing end of the print sheet **10** is located right below the nozzle **121** as shown in FIGS. **11**A and **11**C, the negative pressure generated by the suction fan **650** generates an airstream passing through the belt holes **165**, and ejected ink droplets **20** are affected by an airstream caused by the suction (hereinafter referred to as a suction airstream W**3**).

Hence, the embodiment includes the function of correcting the ejection timing to cope with the suction airstream W**3** in accordance with the position of the print sheet **10** being conveyed right below the nozzle **121**.

First of all, as shown in FIG. **12**, the correction judgment unit **333***c* of the image processing unit **333** judges whether or not a pixel portion onto which ink is to be ejected is inside either the leading end area A**1** or the trailing end area A**2** of the print sheet **10**. As described later, a width L**21** of each of the leading end area A**1** and the trailing end area A**2** is determined as being equal to a distance L**22** between a side surface **120***a* of the ink head and each nozzle **121**.

For example, as shown in FIG. **13**A, if the leading end of the print sheet **10** has not yet reached the side surface **120***a* located on the downstream side of the ink head **120** in the conveyance direction, the distance between the leading end of the print sheet **10** and a position P**1** located right below the nozzle **121** is equal to or smaller than the predefined distance L**22**.

In this case, an airstream which flows downward through the belt holes **165** located below the ink head **120** is generated, which makes the air flow into the holes from the upstream and downstream in the conveyance direction. As a result, ink droplets **20** ejected from the nozzle **121** are affected by the suction airstream W**3**.

On the other hand, as shown in FIG. **13**B, if the leading end of the print sheet **10** has already reached the side surface **120** located on the downstream side of the ink head **120** in the conveyance direction, the distance between the leading end of the print sheet **10** and the position P**1** located right below the nozzle **121** is equal to or larger than the predetermined distance L**22**.

In this case, all of the belt holes **165** located below the ink head **120** are closed. In such a case, the air flows into the belt holes **165** located outside the ink head **120** from a space where no ink head **120** is located, and thus no suction function works on a space below the ink head **120**. As a result, ink droplets **20** ejected from the nozzle **121** are not affected by the suction airstream W**3**.

The description has been given above of the fact that the influence which ink droplets **20** ejected from the nozzle **121** receive from the suction airstream W**3** varies depending on the positional relationship between the leading end of the print sheet **10** and the side surface **120***a* located on the downstream side of the ink head **120** in the conveyance direction; however, a similar variation occurs depending on the positional relationship between the trailing end of the print sheet **10** and the side surface **120***a* located on the upstream side of the ink head **120** in the conveyance direction as well.

Specifically, the influence which ink droplets **20** ejected from the nozzle **121** receive from the suction airstream W**3** varies depending on which position the nozzle **121** for ejecting ink is in among the leading end area A**1** of the print sheet **10**, the trailing end area A**2** of the print sheet **10**, and the central area A**3** other than the leading end area A**1** and the trailing end area A**2** of the print sheet **10**.

Accordingly, in the embodiment, the width of each of the leading end area A**1** and the trailing end area A**2** in which ink droplets **20** ejected from the nozzle **121** are affected by the suction airstream W**3** is determined as the distance L**22** between the side surface **120***a* of the ink head **120** and each nozzle **121**.

In the embodiment, the distance between the side surface **120***a* of the ink head **120** and the nozzle **121** is 15 mm. Whether a pixel portion onto which ink is to be ejected is within an area of 15 mm from the leading end or the trailing end of the print sheet **10** may be acquired from a sensor provided on the conveyance path or instead maybe obtained from the conveyance condition of the print sheet **10**, for example.

The correction judgment unit **333***c* judges that the leading end area A**1** and the trailing end area A**2** of the print sheet **10** are the areas to be affected by the airstream caused by the suction, and that the correction to the ejection timing due to the suction needs be made in these areas. On the other hand, the correction judgment unit **333***c* judges that the central area A**3** other than the leading end area A**1** and the trailing end area A**2** of the print sheet **10** is the area not to be affected by the airstream caused by the suction, and that no correction to the ejection timing due to the suction needs to be made in this area, and performs control such as that in the first embodiment.

Next, a description is given of the correction to the ejection timing due to the suction in the leading end area A**1** and the trailing end area A**2** of a print sheet **10**. FIG. **14** is a graph showing a variation in the amount of landing deviation

depending on a distance between the end portion of the print sheet **10** and a pixel right below a nozzle **121** according to the embodiment. FIG. **15**A is an explanation diagram showing trajectories of ink droplets before and after the correction to the ejection timing due to the suction airstream W**3** is made, in the case where the leading end area A**1** of the print sheet **10** is located right below the nozzle **121**. FIG. **15**B is an explanation diagram showing trajectories of ink droplets before and after the correction to the ejection timing due to the suction airstream W**3** is made, in the case where the trailing end area A**2** of the print sheet **10** is located right below the nozzle **121**.

In the embodiment, the storage unit **334** stores therein suction profile data, as shown in FIG. **14**, indicating the amount of landing deviation caused by the influence of the suction airstream W**3**, with respect to the distance between an end portion of the print sheet **10** and the position P**1** right below the nozzle **121**.

The correction time calculation unit **333***d* calculates the distance between the end portion of the print sheet **10** and a pixel portion on which ink is to be ejected, upon receiving, from the correction judgment unit **333***c*, the result of judgment that correction due to the suction airstream W**3** should be made. Then, the correction time calculation unit **333***d* obtains the amount of landing deviation associated with the calculated distance with reference to the suction profile data. After that, based on the amount of landing deviation thus obtained, the correction time calculation unit **333***d* first calculates, as a correction time Δt**2**, the amount of change to be made to the default correction amount, which the ejection control unit **333***b* uses for the ejection timing correction, the amount of change corresponding to the amount of variation in the amount of landing deviation due to the influence of the suction airstream W**3**.

The correction time Δt**2** (unit: [μs]) is obtained by the following equation (EQ2):

$$\Delta t2=g(y))/v \quad \text{(EQ2)}$$

where g(y) indicates the amount of landing deviation corresponding to the distance y from the end portion of the print sheet **10**, and v indicates the conveyance speed of the platen belt **160**.

Then, the correction time calculation unit **333***d* calculates a correction time Δt for controlling the overall ejection timing with the influence of all of the conveyance airstream W**1**, the self-produced airstream W**2**, and the suction airstream W**3** included. In this event, because the direction of the suction airstream W**3** is different between the leading end area A**1** and the trailing end area A**2** of the print sheet **10**, correction times Δt to be employed in these areas are respectively calculated.

To be more specific, in the leading end area A**1** of the print sheet **10**, ink droplets before the correction of the ejection timing are drifted downstream in the conveyance direction to a large extent as shown by a trajectory T**12** of FIG. **15**A because the conveyance airstream W**1** and the suction airstream W**3** flow in the same direction in this area. For this reason, the correction time calculation unit **333***d* obtains the correction time Δt from the following mathematical formula by using the correction time Δt**1** obtained by the equation (EQ1) and the correction time Δt**2** obtained by the equation (EQ2):

$$\Delta t=\Delta t1+\Delta t2.$$

The correction time calculation unit **333***d* transmits the correction time Δt to the ejection control unit **333***b* as correction data.

Based on the correction data (correction time Δt), the ejection control unit **333***b* performs correction such that the ejection timing at which the landing deviation occurs is moved forward or delayed so that ink droplets follow a trajectory T**11** of FIG. **15**A, which is a trajectory in the case of no suction airstream W**3**, and inputs the corrected signal to the ink head **120**.

On the other hand, in the trailing end area A**2** of the print sheet **10**, ink droplets before the correction of the ejection timing are drifted upstream in the conveyance direction as shown by a trajectory T**22** of FIG. **15**B because the conveyance airstream W**1** and the suction airstream W**3** flow in opposite directions in this area. For this reason, the correction time calculation unit **333***d* obtains the correction time Δt from the following mathematical formula by using the correction time Δt**1** obtained by the equation (EQ1) and the correction time Δt**2** obtained by the equation (EQ2):

$$\Delta t=\Delta t1-\Delta t2.$$

The correction time calculation unit **333***d* transmits the correction time Δt to the ejection control unit **333***b* as correction data.

Based on the correction data (correction time Δt), the ejection control unit **333***b* performs correction such that the ejection timing at which the landing deviation occurs is moved forward or delayed so that ink droplets follow a trajectory T**21** of FIG. **15**B, which is a trajectory in the case of no suction airstream W**3**, and inputs the corrected signal to the ink head **120**

Note that the correction judgment unit **333***c* selects each pixel from the leading end of the print sheet **10** and judges whether or not the pixel is the target of correction due to the suction airstream W**3**; however, the judgment processing on whether or not each pixel is the target of correction due to the suction airstream W**3** may be omitted if it is judged, as a result of analysis of a print image, that the leading end area A**1** and the trailing end area A**2** are blank portions and therefore no print processing needs to be executed in these areas.

According to the second embodiment described above, in addition to the correction to the ink ejection timing to cope with the conveyance airstream W**1** and the self-produced airstream W**3**, the landing deviation in the leading end area A**1** and the trailing end area A**2** of the print sheet **10** due to the influence of the suction airstream W**3** can also be resolved. Thereby, every ejected droplet can be made to land at an appropriate position irrespective of whether the droplet is influenced by the self-produced airstream W**2** and the suction airstream W**3** constantly. As a result, the landing position accuracy can be improved, and a good image free from landing deviation can be provided.

Although the embodiments of the present invention have been described so far, these embodiments are merely examples for making the present invention easy to understand, and the present invention is not limited to the embodiments. The technical scope of the present invention includes not only the specific technical matters disclosed in the above embodiments, but also various modifications, changes, and alternative techniques that can be easily drawn therefrom.

This application claims priority based on Japanese Patent Application No. 2012-137695 filed on Jun. 19, 2012, the entire contents of which are incorporated herein by reference.

According to the present invention, the landing position accuracy can be improved, and a good image free from landing deviation can be formed by resolving the influence of the conveyance airstream and the self-produced airstream which are generated below the ink heads when ink droplets are ejected from the nozzles.

DESCRIPTION OF REFERENCE NUMERALS OR SYMBOLS

10 print sheet
100 inkjet recording apparatus
110 head unit
111 main-scanning flow path
112 sub-scanning flow path
120 ink head
120*a* side surface of ink head (its side surface on upstream side in conveyance direction, its side surface on downstream side in conveyance direction)
121 nozzle
122, **125** ink droplet
150 discharge port
160 platen belt
161 drive roller
162 driven roller
165 belt hole
240 register roller
330 processing unit
331 job data reception unit
332 drive control unit
332*a* head gap control unit
333 image processing unit
333*a* color conversion circuit
333*b* ejection control unit
333*c* correction judgment unit
333*d* correction time calculation unit
334 storage unit
335 sheet type acquisition unit
336 manipulation signal acquisition unit
350 drive unit
350*a* head gap adjustment unit
361 manipulation panel
500 head holder
500*a* head holder surface
500*b* attachment opening
510 stepped guide roller
510*a* upstream guide roller
510*b* downstream guide roller
620 platen plate
622 suction hole
650 suction fan
A**1** leading end area
A**2** trailing end area
A**3** central area
D**1** unit line
E**1** certain nozzle
W**1** conveyance airstream
W**2** self-produced airstream
W**3** suction airstream

What is claimed is:

1. An image formation apparatus configured to, when forming an image by ejecting ink from nozzles of an ink head onto a recording medium being conveyed on a conveyance path, control timing of ink ejection from each of the nozzles to cope with a conveyance airstream generated by the conveyance of the recording medium, the apparatus comprising

an adjustment unit configured to adjust the ejection timing control on the basis of a self-produced airstream rate which is calculated based on a volume of ink ejected from the nozzle per unit time and indicates a generation rate of a self-produced airstream that causes the ink ejected from the nozzle to go straight against the conveyance airstream,

a storage unit configured to store profile data in which the number of ink ejections from the nozzle per unit time and an amount of landing deviation of ink on the recording medium are associated with each other; and

a judgment unit configured to judge whether or not the adjustment to the ejection timing control is needed, on the basis of a result of comparison between the volume of ink ejected from the nozzle per unit time and an ink ejection volume threshold corresponding to the self-produced airstream rate, wherein

for the nozzle determined as needing the adjustment to the ejection timing control by the judgment unit, the adjustment unit calculates the number of ink ejections from the nozzle per unit time from the volume of ink ejected from the nozzle per unit time, determines an amount of landing deviation of ink corresponding to the calculated number of ink ejections on the basis of the profile data, and adjusts the ejection timing control using an adjustment content determined based on the self-produced airstream rate corresponding to the determined amount of landing deviation.

2. The image formation apparatus according to claim **1**, wherein the judgment unit

judges whether or not the nozzle has ejected at least one drop of ink to each of a predetermined number of pixels consecutively located on the recording medium at a position downstream of the nozzle in a conveyance direction of the recording medium, as the result of comparison between the volume of ink ejected per unit time and the threshold, and

judges that the adjustment to the ejection timing control on the nozzle is needed if judging that the nozzle has ejected at least one drop of ink to each of the pixels.

3. The image formation apparatus according to claim **1**, further comprising:

a sheet type acquisition unit configured to acquire information on a thickness of the recording medium; and

a drive control unit configured to change a distance between the conveyance path and an ejection surface of the nozzle on the basis of the information on the thickness acquired by the sheet type acquisition unit, wherein

the storage unit stores a plurality of the profile data corresponding to the distance, and

the adjustment unit adjusts the ejection timing control using an adjustment content depending on the distance changed by the drive control unit.

4. The image formation apparatus according to claim **2**, further comprising:

a sheet type acquisition unit configured to acquire information on a thickness of the recording medium; and

a drive control unit configured to change a distance between the conveyance path and an ejection surface of the nozzle on the basis of the information on the thickness acquired by the sheet type acquisition unit, wherein

the storage unit stores a plurality of the profile data corresponding to the distance, and

the adjustment unit adjusts the ejection timing control using an adjustment content depending on the distance changed by the drive control unit.

5. The image formation apparatus according to claim **4**, further comprising

a suction unit configured to suck the recording medium to the conveyance path, wherein

when the nozzle is located in an area within a predetermined distance from any of a leading end and a trailing

end of the recording medium, the adjustment unit adjusts the ejection timing control depending on an airstream caused by the suction unit.

6. An image formation apparatus configured to, when forming an image by ejecting ink from nozzles of an ink head onto a recording medium being conveyed on a conveyance path, control timing of ink ejection from each of the nozzles to cope with a conveyance airstream generated by the conveyance of the recording medium, the apparatus comprising

an adjustment unit configured to adjust the ejection timing control on the basis of a self-produced airstream rate which is calculated based on a volume of ink ejected from the nozzle per unit time and indicates a generation rate of a self-produced airstream that causes the ink ejected from the nozzle to go straight against the conveyance airstream,

a suction unit configured to suck the recording medium to the conveyance path, wherein

when the nozzle is located in an area within a predetermined distance from any of a leading end and a trailing end of the recording medium, the adjustment unit adjusts the ejection timing control depending on an airstream caused by the suction unit.

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